

CFD analysis of the ventilation heating system

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Abstract. Air conditioning is a significant part of the contemporary life. A lot of the medical papers confirmed the influence of the thermal comfort to the operability. The aim of the article is to understand the system of the building ventilation with the HRV unit. For this purpose, the CFD simulation model was elaborated. The ANSYS Fluent allows to calculate the heat balance of the room with secondary thermal gains like computers, monitors and humans. The results of the simulation approved that in the modern thermal passive houses heat balance calculations should take into account secondary thermal gains from the installed equipment. Also the air circulation in the closed area and the influence of the different barriers installed in the laboratory were investigated.

Keywords: CFD / Fluent / ventilation / HRV

1 Introduction

Ventilation in homes, flats and in offices is very important, especially because of health and hygienic-housing ensuring optimum moisture and e.g. mould occurrence.

According to the norms that normal window ventilation is sufficient and hygienic, if window is open for about an hour a day. Of course, with such ventilation, a considerable amount of heat will be lost, about 50%.

Due to this, managed ventilation systems have been developed to optimize the need for air exchange in residential areas. Units of controlled ventilation contain a heat exchanger that enables heat recovery to reduce the loss of heat and save housing costs. It is very difficult (if not impossible) to build modern passive house without installing air recuperation systems or Heat Recovery Ventilators (HRV) [1–8].

In the heat balance calculation, it is necessary to know all heat losses and thermal gains. In a modern passive building the heat losses are small, approximately 2–3 kW per 100 m². According to this, heat balance calculation should expand by the thermal gains positions which were not present before, for example heat from the working electrical equipment or human body [9–11].

People lose heat in the following proportion:

- 35% by heat conduction and convection;
- 35% by thermal radiation;
- 24% by evaporation;
- 6% by breathing.

Nevertheless, for the private houses these are still very low numbers but in the offices where 2–3 peoples are working on the computers it is enough to change the heat balance [12–14].

In the current article the air ventilation in the laboratory using of HRV and floor radiators in winter conditions with the impact of the small thermal gains such as computers and human body was simulated.

2 Materials and methods

Room under the study was a laboratory of the renewable energy sources of the Technical University in Kosice [15]. The technical drawing of the laboratory shown in Figure 1.

In the laboratory there are situated three thermal storage tanks for the hot and cold water for heating and cooling purposes in the summer period. The ventilation of the laboratory is going through ventilation canals in the upper part of the room. Fresh air comes to the laboratory via canal 1 and goes out through the canal 2. As you can see from the picture first air canal has two nozzles while the second air canal has three situated approximately at the middle of each the windows. The HRV unit (Sabiana ENY 3) is situated in the room next door (Fig. 2). The configuration of ENY 3 allows preheating fresh air in winter period by hot water or integrated electric heater when heat potential of exhaust air is not enough or intensity of ventilation is high [15].

The regulation equipment is totally controlled by the DESIGO by Siemens. View on the DESIGO program is shown in Figure 3. At the right side of

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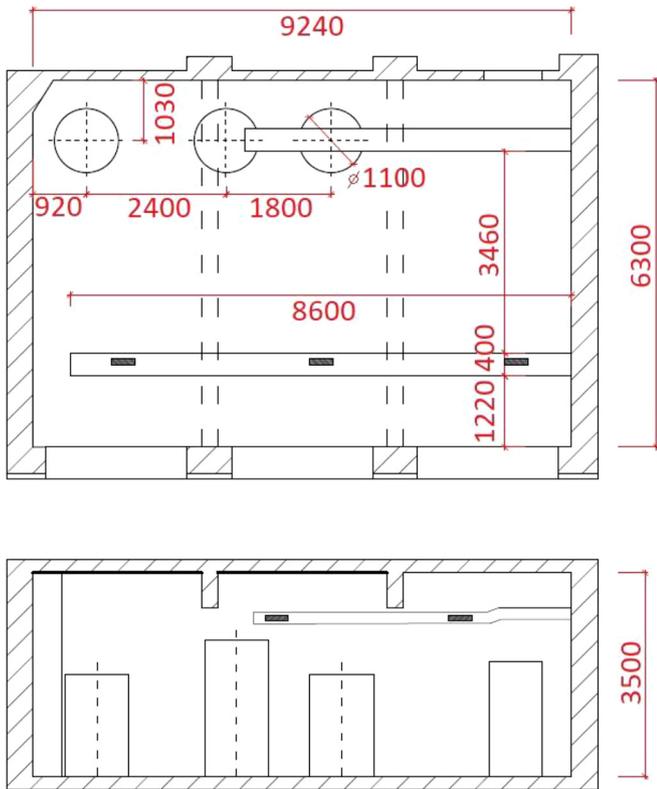


Fig. 1. Laboratory under the study.



Fig. 2. Sabiana ENY 3.

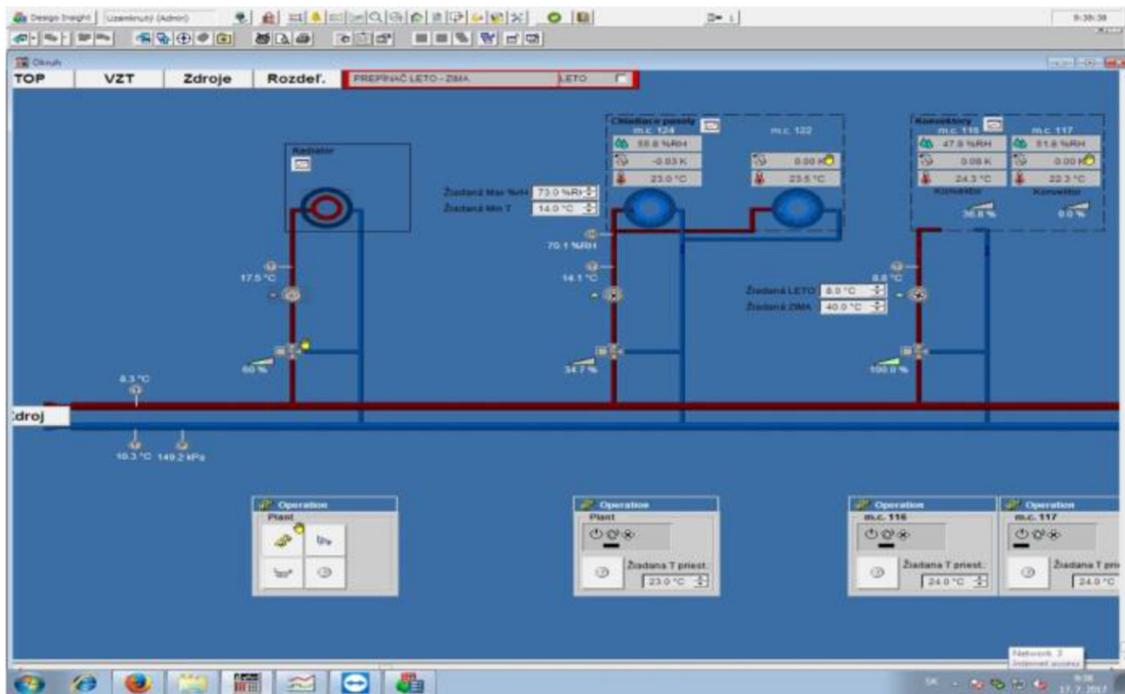


Fig. 3. DESIGO program.

the figure is illustrated the control panel of the thermal parameters of the rooms with installed floor convectors and heat recuperation system. Due to the DESIGO and installed measure equipment it is possible to control temperature and humidity. Also the CO concentration is monitored. Despite the fact that heat equipment is installed in two rooms the DESIGO allows to setup the thermal and humidity parameters in the itch room separately [15].

The input parameters were the same comparing with the article of prof. M. Rimar “Study of gaseous flows in closed area with forced ventilation” (SGFCAFV) and 14.

According to EN 12831 the temperature in the laboratory must be 20°C.

Thermal characteristics of the windows, walls, floor and ceiling were chosen according to their technical documentation.

Sickness of internal walls is 200 mm and temperature is 22°C.

External wall has 500 mm sickness and temperature in the middle of the wall is 18°C.

Sickness of windows is 100 mm and external surface temperature is 12°C.

Ceiling and floor have 300 mm sickness and 22°C temperature.

The main source of heat in the laboratory is two floor radiators which are installed under the windows. The surface temperature of radiators is 42–45°C in winter period. It is impossible to complete turn off the heating of the laboratory as through these floor radiators is going the whole heat to the building. Also heat achieved through the thermal storage tanks. The tanks are isolated by special fibrous material of 10 cm sickness. The surface temperature during the day of the first tank (in the corner) is around 24.5°C, second – 23.5°C, third – 22°C. The temperature of hot water inside the tanks is approximately 37.5°C for the first tank, 32°C – second, 25°C – third. Also at the picture you can see six tables with computers and monitors. Computer boxes which are situated under the table are the working station so they have higher energy consumption and as a result higher thermal gains – 100 W/m². This parameter was chosen to simplify the simulation model. The thermal gains from the monitors are 50 W/m². Two cube models in front of the tables are the simplified models of the sitting human bodies. The surface temperature of the human model was 36°C [15].

3D model was made in ANSYS design modeler to provide stable calculation and to eliminate inaccuracy in the geometry. ANSYS mesh solver was chosen for the mesh making purpose to reach the better quality. Proximity and curvature advanced size function with fine relevance centre, active assembly initial size seed, high smoothing and slow transition also was used for these purpose. According to the settings model had 2,958,471 elements what is by 45% higher comparing the model without tables, computers and people [15].

3 Results

Simulation of the heating and ventilation was made in ANSYS Fluent 14.0. As a setting for FLUENT was used

energy equation model, standard K-epsilon model and radiation p1 model. Inlet type was chosen as velocity-inlet with velocity magnitude 0.2 m/s and 19°C. For outlet was pressure outlet type. All the parameters were chosen according to the technical documentation of the HRV and the norm of the thermal comfort. The research of the heat recovery parameters of the ENY 3 is not a purpose of the current work. The results of the simulation are on the picture. At the picture illustrated the streamlines of fresh inlet air and temperature contours of the laboratory (Fig. 4).

These simulations confirm the results of the previews research SGFCAFV. The main reasons of the turbulent stream at the half of the laboratory are the shape of the nozzles and the ventilation canal also as a velocity of the air. The maximum velocity of the fresh air is 0.36 m/s what is under the limits of EN 12831. At the down part of the picture illustrated temperature contours of walls, windows and floor radiators.

Comparing with the model in the previews article SGFCAFV current model has some differences in the down half of the laboratory. This is caused not only by presence of the barriers like tables and humans but also and extra heat sources like computer and monitors. The temperature difference in the vertical axis of the room is 0.7°C/m what is appropriate according to the EN 12831.

Relatively warm fresh air from the HRV comes to the upper part of the laboratory. It encounters to the cold windows and fall down as its temperature reduce. In the down part of the windows warm air near radiators mixing with falling cool air. Than air flow divides by two streams. The first one (warmest) goes up and after mixing with warm extract air exhaust through outlet canal. The second one (coldest) circulate in the down part of the laboratory where it cooling the computers and monitors and after it heats goes up through outlet canals.

According to the simulation the internal temperature in the laboratory is 23–24°C depending on the high. The internal temperature according to the thermometers is 24°C (Fig. 5). The difference between the values is caused by the fact that when was set the parameters of wall heat transfer were not considering with thin layers of the wall like paint. The surface temperatures of the computers and monitors are 45°C and 41°C respectively.

The simulation shows the high accuracy with the measured data especially in the period between 10 AM and 16 PM. The difference in the data on the other periods can be explained by the transient thermal processes during the day while the simulation was steady in itch time segment.

Also was made simulation of the air ventilation in the laboratory with turned off the heating from radiators (Fig. 6).

According to this simulation the internal temperature in the laboratory is 21.5–23.4°C depending on the high. Such slight difference between the values in the first and second simulations is caused by the thermal gain from the next rooms. The temperature difference in the vertical axis of the room is 1.1°C/m what is very close to the limit according to the EN 12831.

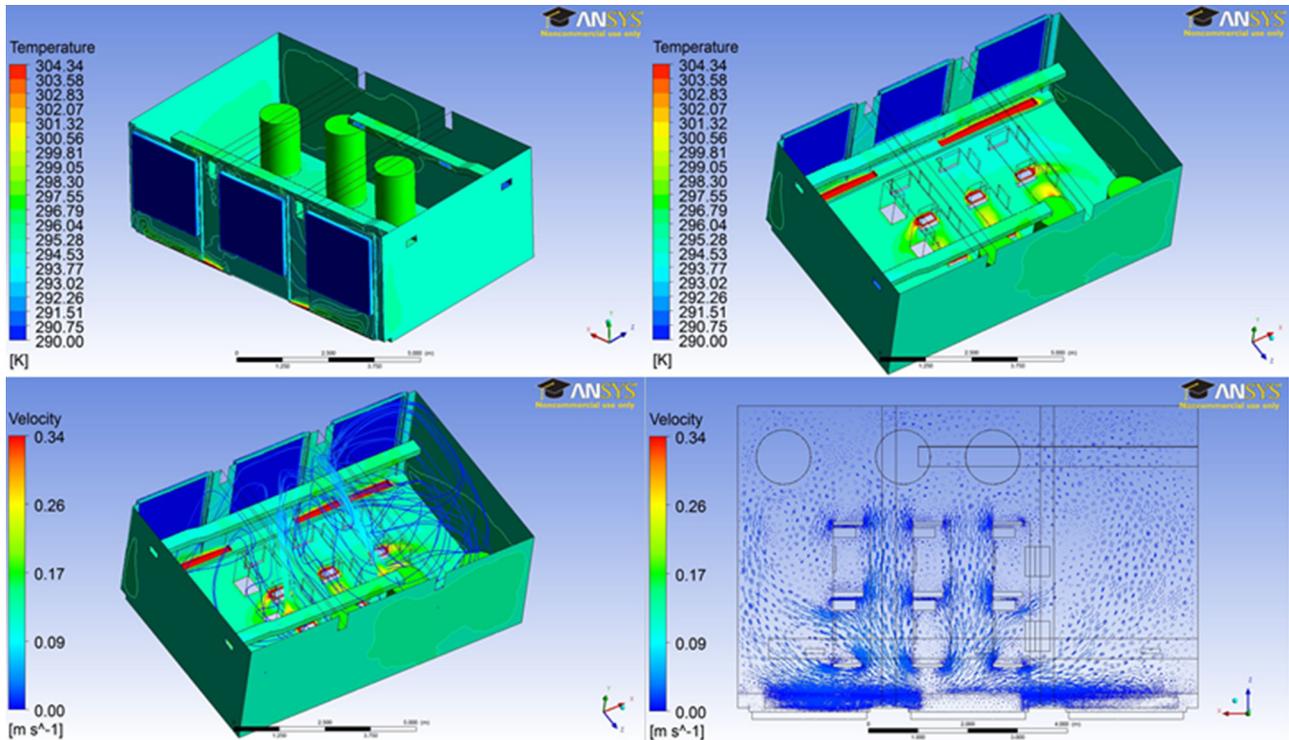


Fig. 4. Results of the first type simulations.

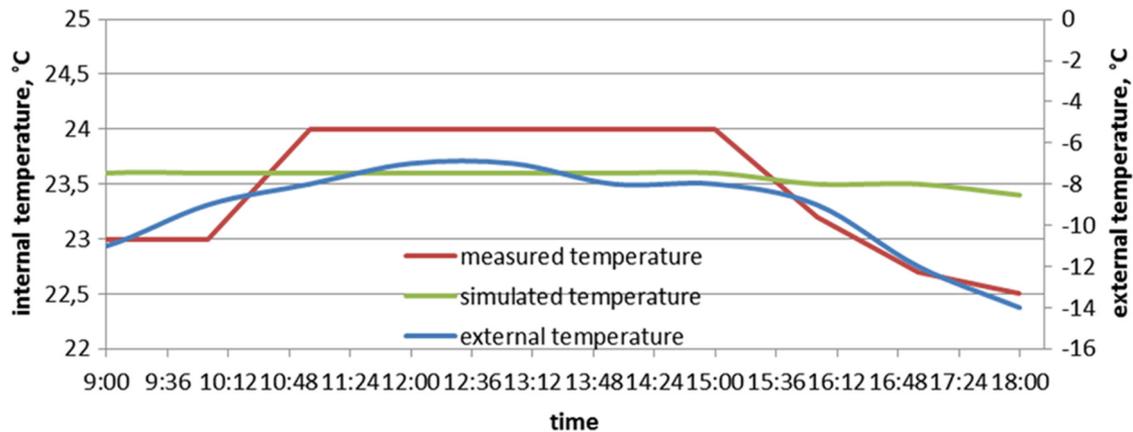


Fig. 5. Comparison of the measured and simulation data.

Reduction of the internal temperature in the laboratory result slightly changes of the air ventilation. The main trends of air circulation are not changed but the path of the coldest air in the down part of the laboratory increased approximately by 15–20%. Also the surface temperatures of the computers and monitors are decreased by 10–15% to 42 °C and 37 °C respectively.

Comparison of the simulation results of the laboratory model with and without tables, computers, monitors and humans is shown in Figure 7.

Air circulation in the down part of the laboratory changed significantly in the model with tables, computers, monitors and humans. Figure 7 presents

turbulent flow in the down part of the room. This flow is caused by the barriers which are situated on the air flow path.

Figure 8 presents air flow in the laboratory without barriers. After the turbulent zone near the windows air flow stabilize and has laminar character of the flow.

4 Discussion

The main idea of the current work was to make simulation and analysis of the influence of the secondary thermal gains in the room on its total heat balance system. Secondary

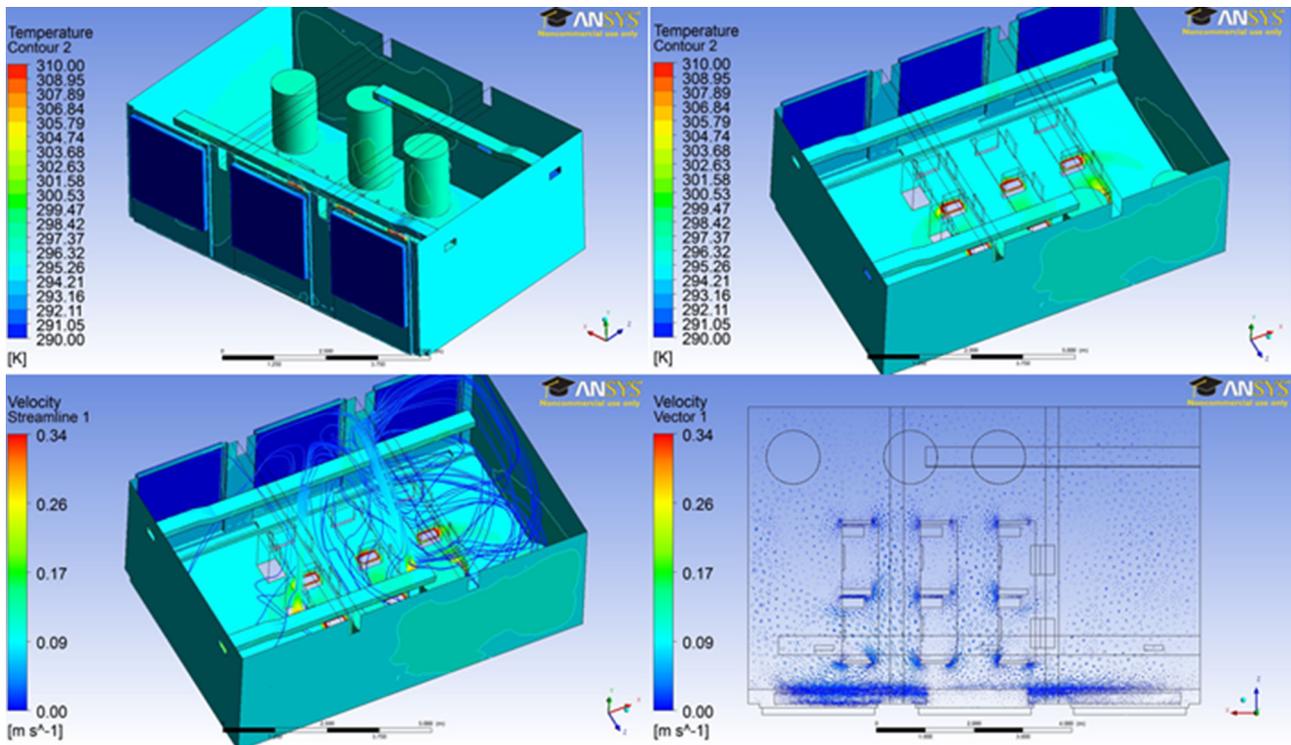


Fig. 6. Results of the first type simulations.

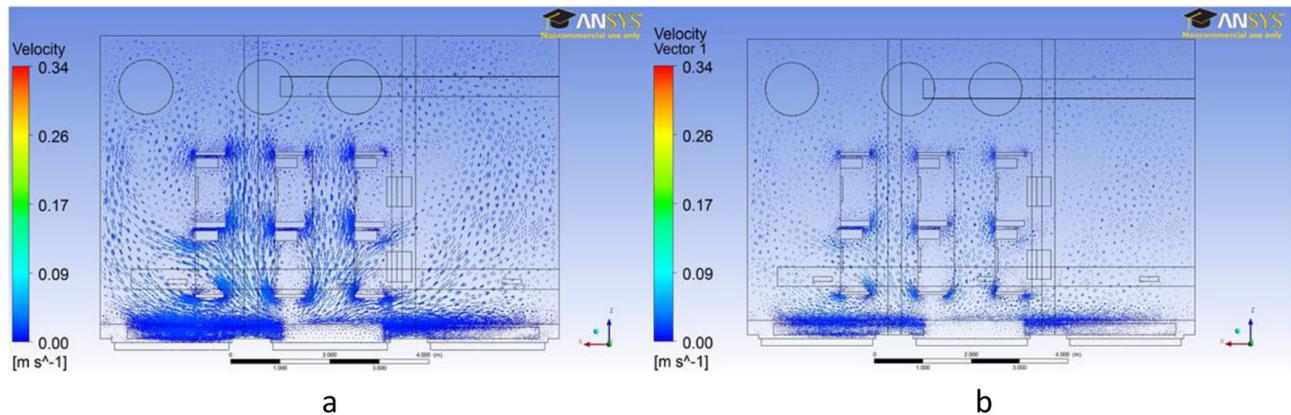


Fig. 7. Air flow in the laboratory with barriers.

thermal gains in the room under the study were computers, monitors and humans. Also was made an analysis of the air ventilation system with heat recovery ventilator. The conclusions of the study are as follows:

1. In the modern buildings which belong to the energy passive standard is necessary to take into account with the secondary thermal gains like computers, monitors or other equipment that produces a waste heat; such waste heat change the heat balance and or should be deliver to other areas or it is necessary to reduce the heating of the current area.
2. Were confirmed the results of the previews research that heating of the room by the only heat

recovery ventilation results higher (more than 2°C) differences of the temperature in the vertical axis of the room.

3. It is necessary to use modern simulation programs to calculate internal climate of the room as one of the major factor which affect the effectiveness of the work in the closed areas with forced ventilation.
4. One of the major benefits of using the CFD simulation software is an ability to calculate and predict the areas of better and worse hydrothermal parameters for the human being due to possibility to calculate all the necessary parameters in every single volume of the simulated object.

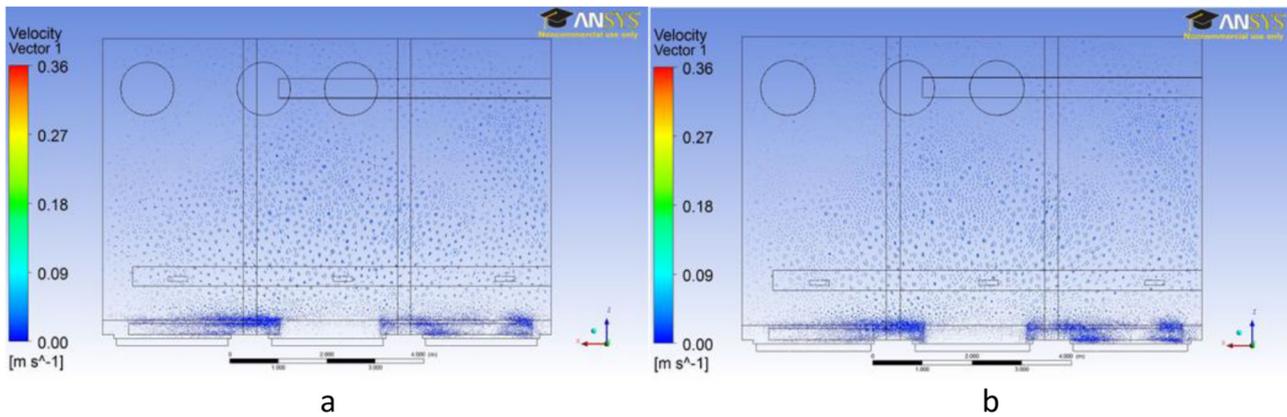


Fig. 8. Air flow in the laboratory without barriers.

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References

- [1] S. Driss et al., *Energy Build.* **119**, 28–40 (2016)
- [2] P. Kalliomaki, P. Saarinen, W. Tang, J.H. Koskela, *Build. Environ.* **25**, 683–693 (2016)
- [3] A. Panda et al., *Appl. Mech. Mater.* **19** (2014)
- [4] J. Zajac, I. Čorny, *Monitoring of processing fluids*, Science Report, Kielce, pp. 215–229, 2004
- [5] D. Micallef, *Energy Build.* **3**, 2016 (2016)
- [6] C. Zhang, P.K. Heiselberg, *Build. Simul.* **10**, 203–218 (2017)
- [7] T.H. Pedersen, K.U. Nielsen et al., *Build. Environ.* **266** (2017)
- [8] K. Hu, Q. Chen, *Build. Environ.* **94**, 676–682 (2015)
- [9] M. Napp, T. Kalamees, *Energy Build.* **96** (2015)
- [10] X. Wu et al., *Energy Build.* **172** (2016)
- [11] T. Mikeska, J. Fan, *Energy Build.* **107** (2015)
- [12] M. Flimel, D. Dupláková, *Appl. Mech. Mater.* **66**, 0308031–3080319 (2014)
- [13] X. Ye, *Build. Environ.* **120**, 1–12 (2017)
- [14] J. Jandacka et al., *Optimization principle of operating parameters of heat exchanger by using CFD simulation*, in *10th Anniversary International Conference on Experimental Fluid Mechanics*, 2015
- [15] M. Rimár et al., *Analysis and Simulation of Forced Ventilation in Special Condition*, in *Proceedings of the XXI. International Scientific Conference, The Application of Experimental and Numerical Methods in Fluid Mechanics and Energy, Zilina, Slovak Republic*, 2018

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